

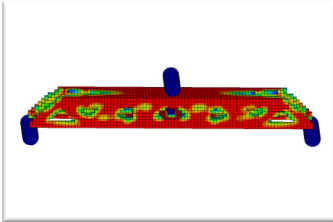
Application of the equivalent static load method for impact problems with GENESIS and LS-DYNA

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DYNAmore GmbH

Heribert Kassegger
MAGNA STEYR Engineering AG & Co KG

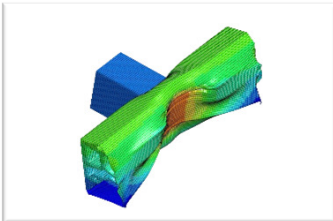
Orlando, FL 24th May 2013
10th World Congress on Structural and
Multidisciplinary Optimization

Outline



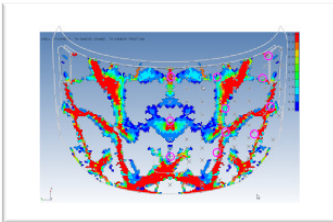
Introduction

Equivalent Static Load Method



Case Study 1

Extrusion Profile Optimization, Research Project Crash-Topo



Case Study 2

Optimization of an Engine Hood



Summary

Conclusions, Lessons Learned

DYNAmore GmbH - Introduction

- Headquarters in Stuttgart (Germany)

- About 80 employees

- Core Products

- LS-DYNA
- LS-OPT, Genesis/ESL
- LS-PrePost



- Business

- Support, consulting, engineering services, programming, training, conferences,...
- Finite Element and optimization software development
- Process integration, SDM
- ...



Overview



Stuttgart [HQ]

Introduction ESL

■ Idea of the Equivalent Static Load Method

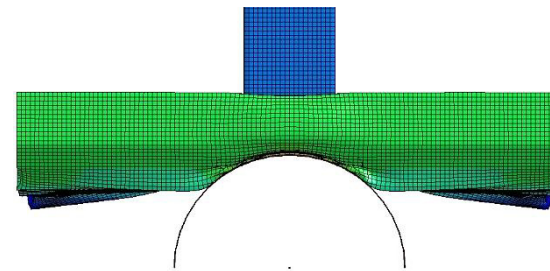
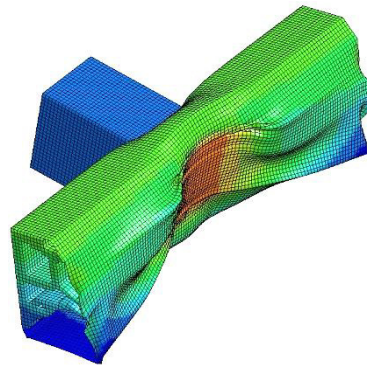
- Decomposition of the nonlinear, dynamic optimization problem in

Nonlinear dynamic analysis → displacement field

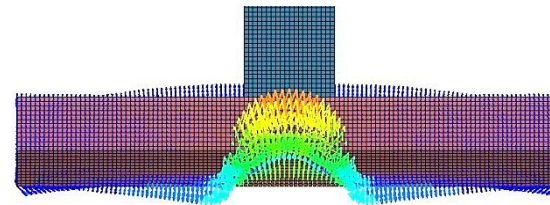
Equivalent static loads for single time steps

„multi load case topology optimization“ with equival. static loads

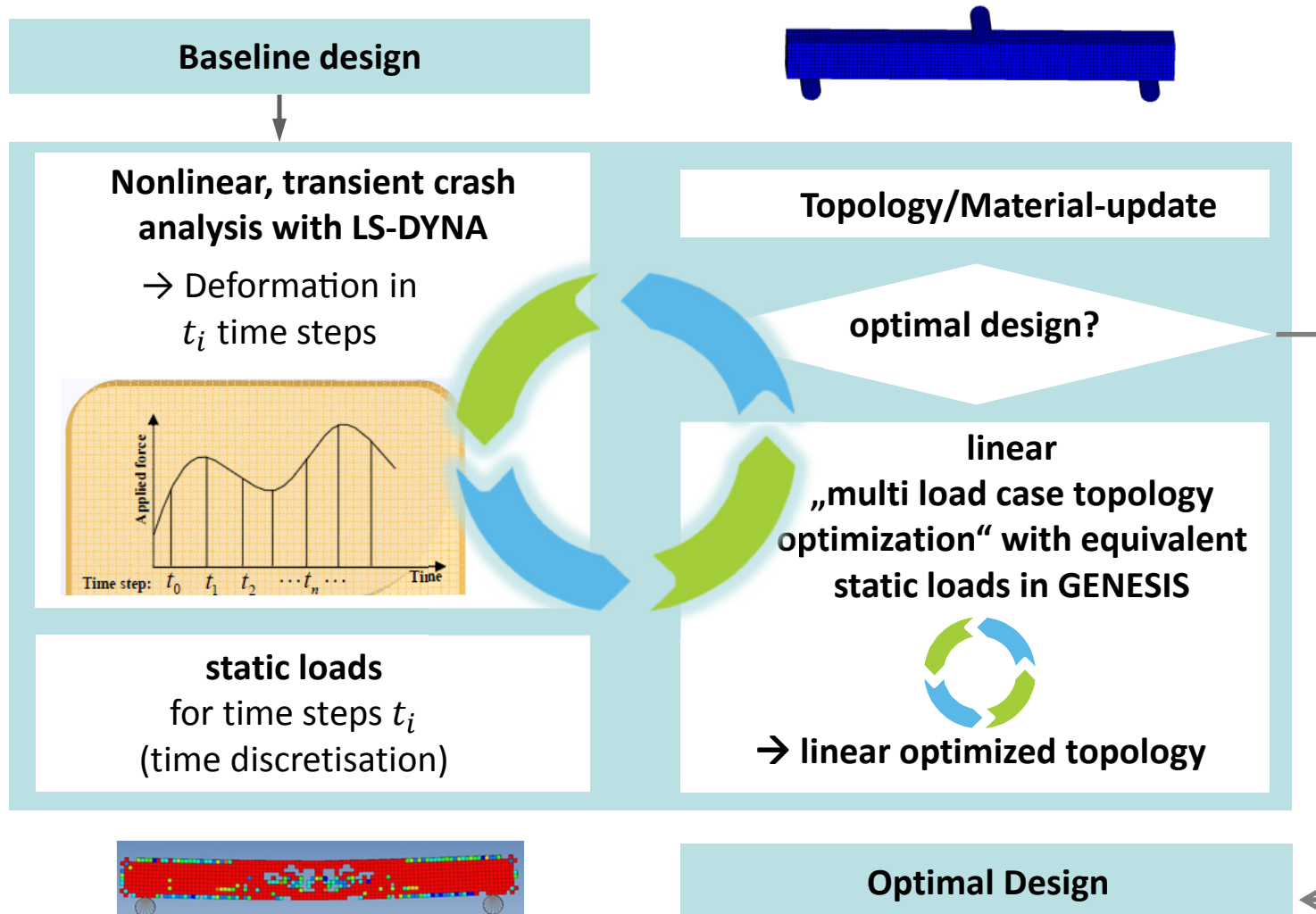
Displacement field:
 $\mathbf{u}_t(\mathbf{x})$



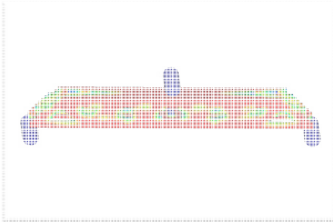
Equivalent static loads:
 $\mathbf{F}_t(\mathbf{x}) = \mathbf{K}_{lin} \mathbf{u}_t(\mathbf{x})$



Introduction ESL

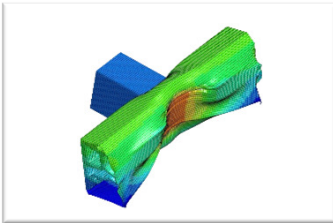


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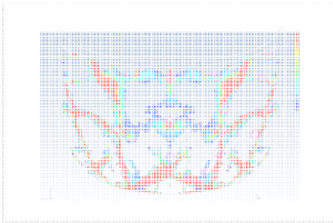
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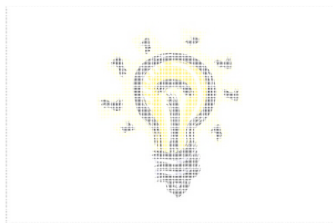
Case Study 1

Extrusion Profile Optimization, Research Project Crash-Topo



Case Study 2

Optimization of an Engine Hood



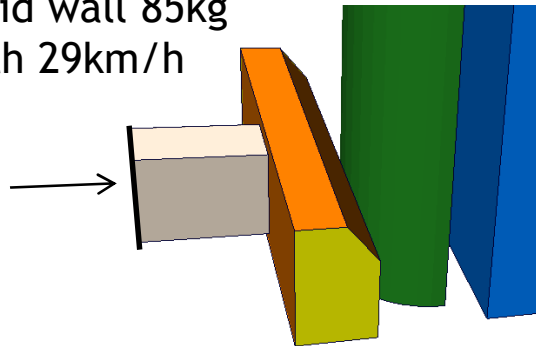
Summary

Conclusions, lessons learned

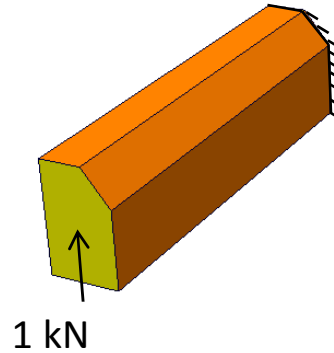
Extrusion Profile Optimization

■ Load Cases

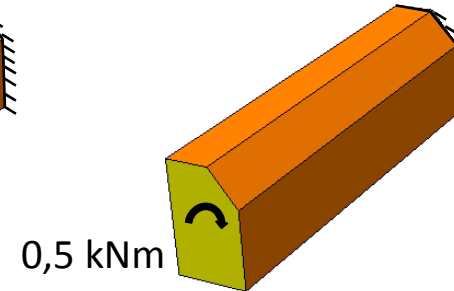
Rigid wall 85kg
with 29km/h



Pole Crash



Bending



Torsion

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■ Targets

- LC Crash: Contact force < 40 kN, time history of contact force as uniform as possible, Intrusion < 70mm
- LC Bending: Displacement < 0.39mm
- LC Torsion: Wrinkling < $3.5 \cdot 10^{-3}$ rad
- Mass < 2.8kg
- 1.6 mm < fillet thickness < 3.5 mm

Extrusion Profile Optimization

■ Objectives

- LC Crash: maximize internal energy
- LC Bending: minimize internal energy
- LC Torsion: minimize internal energy

■ Constraints

- LC Crash: Intrusion < 70mm
- LC Bending: Displacement < 0.3867mm
- LC Torsion: Wrinkling < $3.554 \cdot 10^{-3}$ rad
- Extrusion constraint

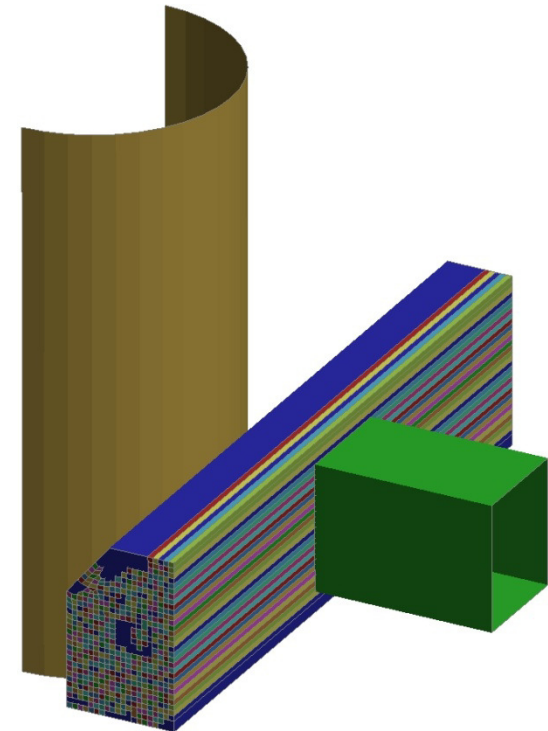
■ Element discretization

- Hexaeder elements with 2mm edge length
- Fully integrated elements

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Extrusion Profile Optimization

■ Result example with ESL-Method

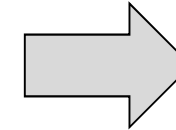
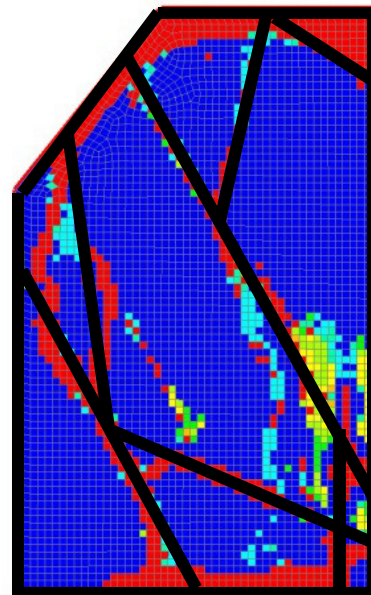
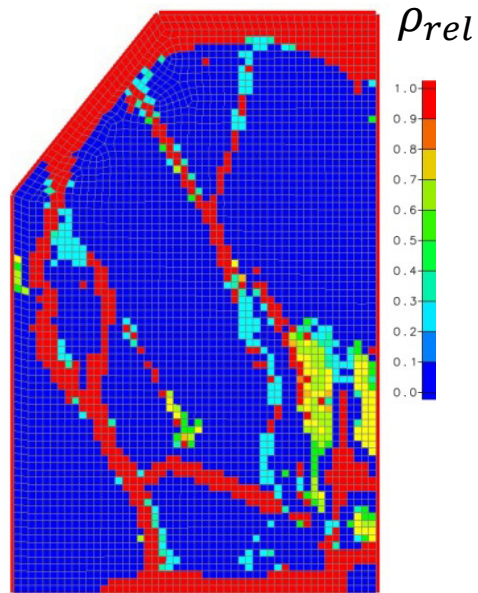
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Optimized relative
density distribution

Possible
interpretation



Results might be transferred to SFE
concept for subsequent shape
optimization with GHT and LS-OPT
- interface has been developed
within research project

Extrusion Profile Optimization

■ Result example with ESL-Method

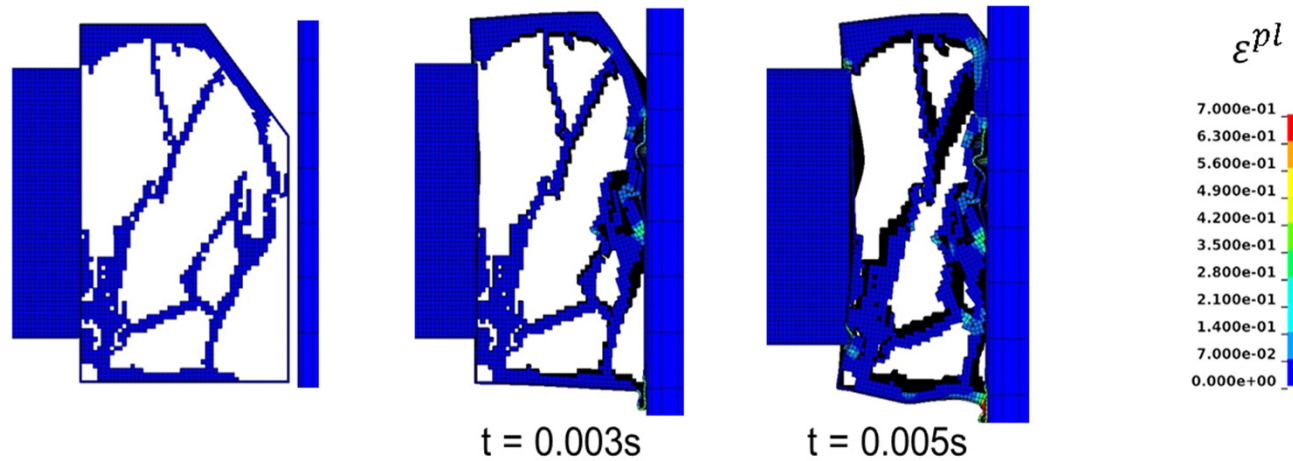
■ Analysis results of optimized topology

- Maximal Intrusion: **67,1 mm** (constraint: $d < 70\text{mm}$)

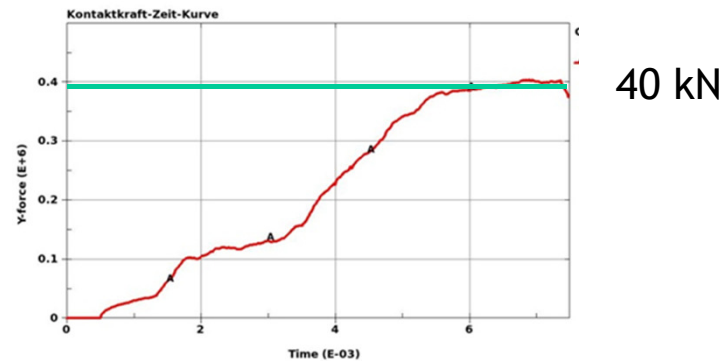
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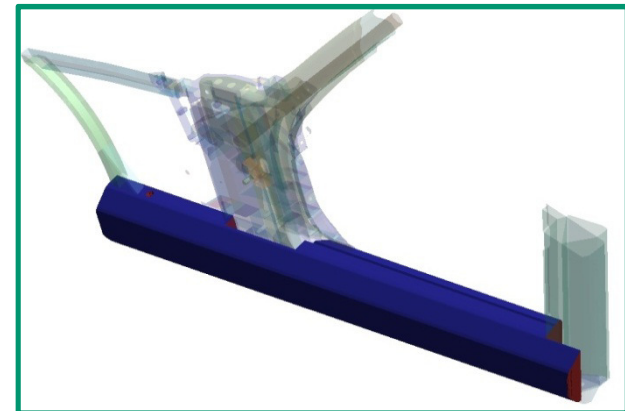


- Maximum contact force: **40,4 kN**

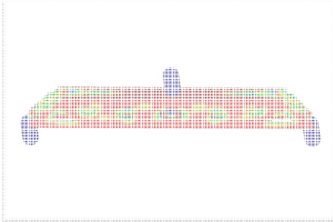


Summary

- Within the research project „Crash Topo“ topology optimization of extrusion profiles, mainly on the example of automotive rocker sills, was examined
- As one new approach for optimization the „Equivalent Static Load Method“ was applied
- An automated process with LS-DYNA and Genesis has been setup on an HPC environment
- Geometry of rocker sills can be very complex → no straight forward extrusion profiles
- Fine resolution (small element size) of solid elements within construction space is required, but lead to many elements (ex.: 1mm el.-length → ~10mio elements)
- Large buckling of fillets lead to limits of ESL method

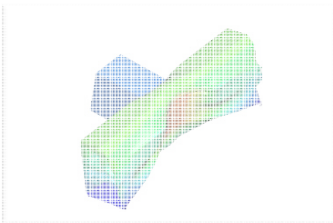


Agenda



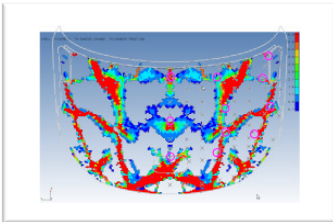
Introduction

Equivalent Static Load Method



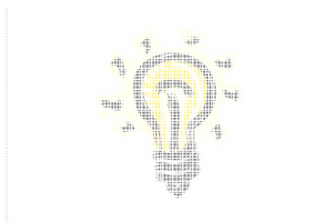
Case Study 1

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Case Study 2

Optimization of an Engine Hood



Summary

Conclusions, lessons learned

■ Project Information

- Joint project between MAGNA STEYR Engineering AG & Co KG and DYNAmore GmbH

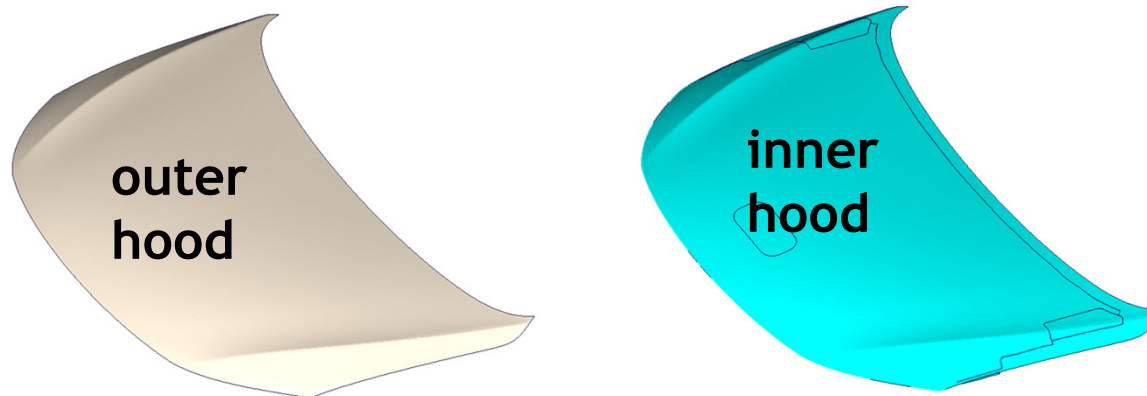
■ Motivation

- Development of a standardized method to design an inner hood panel
- Method should be able to take into account different package and geometry conditions
- Main load cases are head impact (pedestrian safety) and stiffness

■ Expected Results

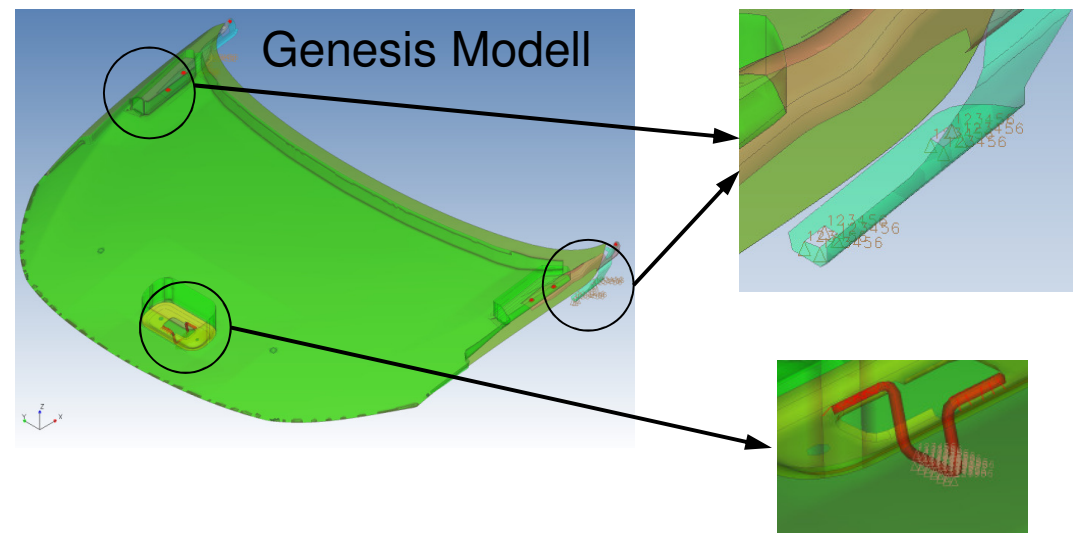
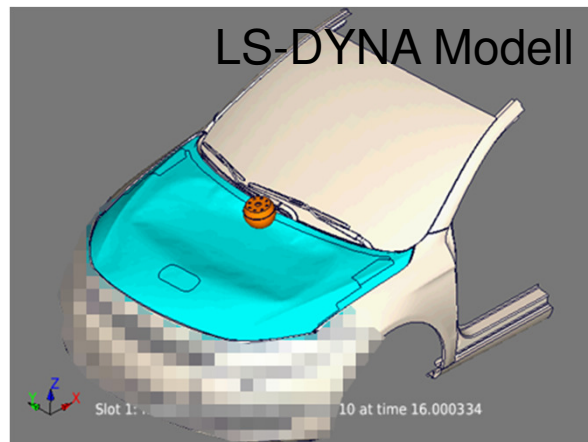
- Design of inner hood panel with optimal HIC-value for head impact and stiffness values for static load cases

- Outer hood with constant shell thickness $t=0,6\text{mm}$ and material H220
- Inner hood is a duplicate of the outer hood with same nodes and coincident elements but separate property with material DX 56D.

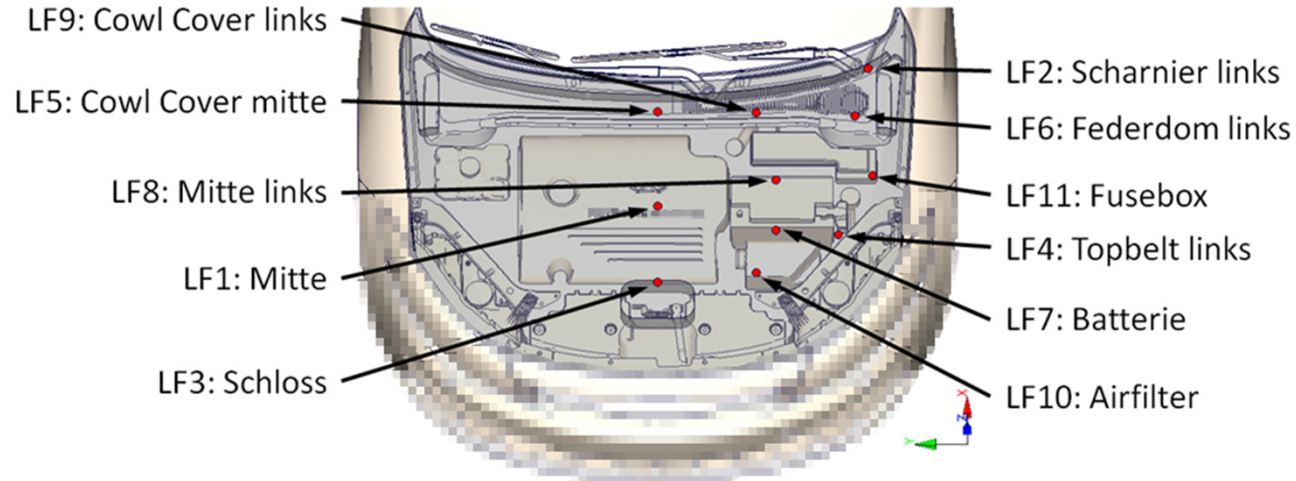


- Design variables for optimization are thicknesses of every single element (Topometry Optimization).
 - Variation of thickness between $0,1\text{mm}$ and $5,0\text{mm}$.
- Reduction of number of variables
 - Clustering of elements \rightarrow 4 neighbouring elements have the same thickness during optimization.
 - Symmetry constraint in y-direction

- **LS-DYNA model for nonlinear impact simulation**
 - reduced car model with blocking package elements in the engine compartment
- **Genesis model for optimization with ESL method**
 - only hood with hinges and lock is considered
 - support with SPC's on the hinges and the lock
 - the preceding LS-DYNA simulation has been discretized with 9 equivalent static load cases ($\Delta t=2$ ms)



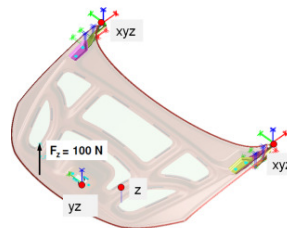
Head impact at 11 points



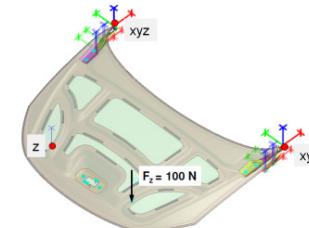
Static loads

- corner bending
- torsion
- bending cross member
- bending longitudinal member

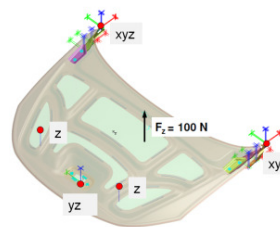
Lastfall: Corner Bending



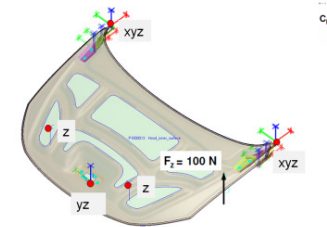
Lastfall: Torsion



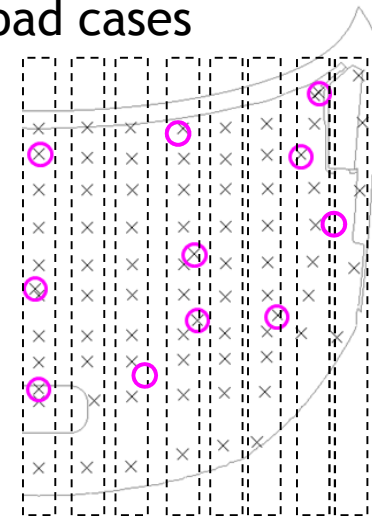
Lastfall: Bending Cross Member



Lastfall: Bending Longitudinal Member



- HIC-Value can not be used as an objective in linear inner topology optimization loop
- Opt. problem formulation for head impact instead
 - Maximize deformation of the hood by avoiding contact with stiff (rigid) underlying structure
- Objective
 - Maximize strain energy for head impact load cases
- Constraints
 - Limits for displacement in z-direction for head impact load cases
 - About 80 points with maximum feasible deformation
 - Only for the ESL load cases with large deformation from 6ms on (7 per head impact point)
 - $11 \text{ (Head impact point)} * 7 \text{ (ESL)} * 80 \text{ (Points with displacement limit)}$
= 6160 (constraints)
 - Limits for displacement of the static load cases



Evaluation of HIC values for each LS-DYNA simulation

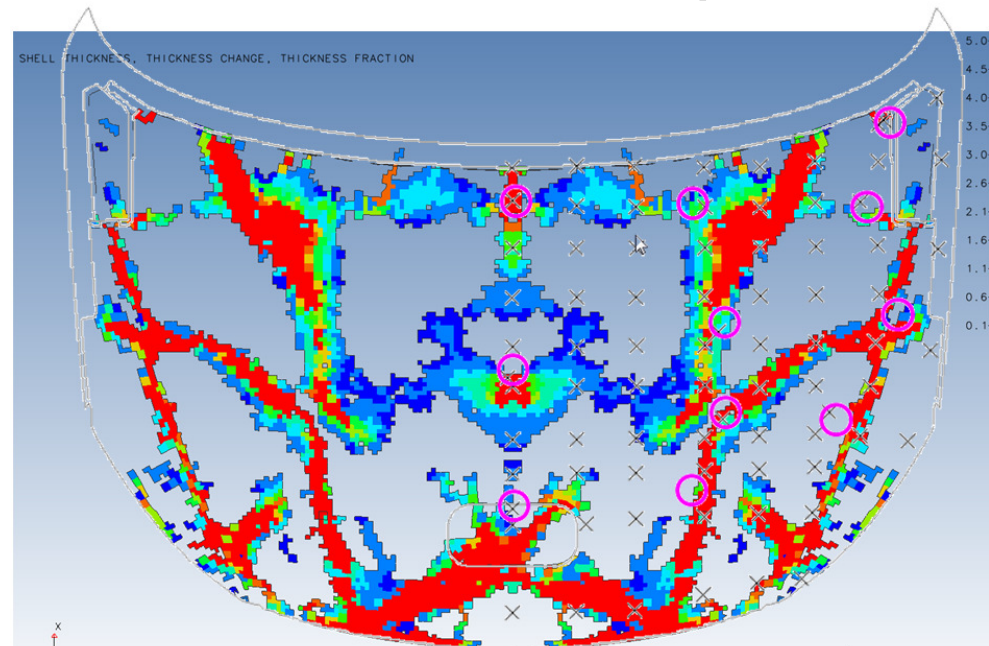
Starting design

Dyna-Rechnung	LF1_Mitte	LF2_Scharnier_li	LF3_Schloss	LF4_Topbelt	LF5_Cowl_Cover	LF6_Federdom	LF7_Batterie	LF8_Mitte_li	LF9_Cowl_li	LF10_Airfilter	LF11_Fusebox	unter 900	900-1000	über 1000	Vmin > 0
0												4	2	3	2

Optimal design

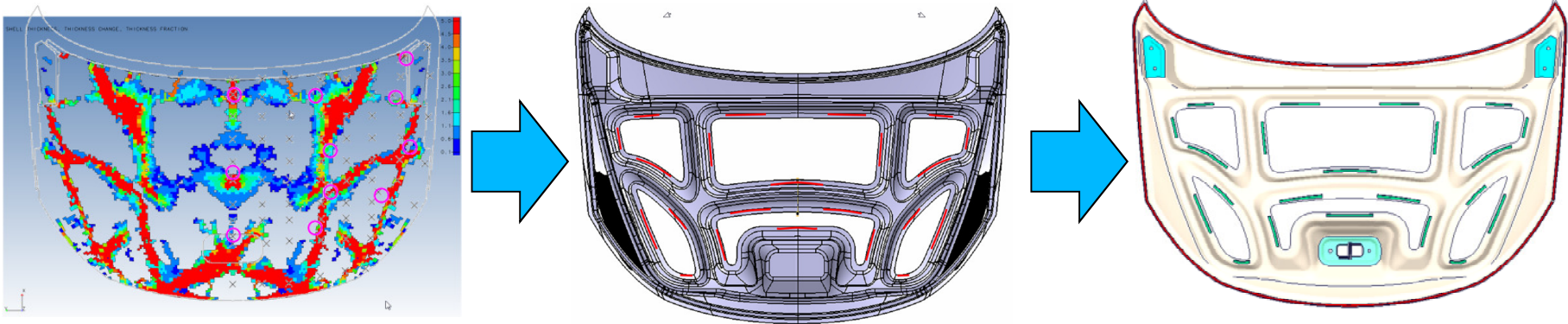
Dyna-Rechnung	LF1_Mitte	LF2_Scharnier_li	LF3_Schloss	LF4_Topbelt	LF5_Cowl_Cover	LF6_Federdom	LF7_Batterie	LF8_Mitte_li	LF9_Cowl_li	LF10_Airfilter	LF11_Fusebox	unter 900	900-1000	über 1000	Vmin > 0
17												8	0	3	0

Element thickness distribution for the optimal solution



Elements with very low thickness are masked

■ Interpretation of CAD-design of the inner hood



■ LS-DYNA simulation results of the final design

■ Head impact, HIC values

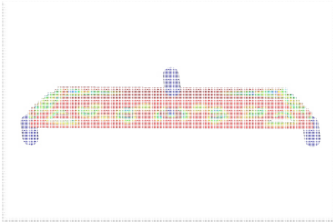
- On average, results of final CAD-design getting a little worse compared to final topometry optimization results

■ Static loadcases

- torsion → threshold value complied
- corner bending → threshold value complied
- bending cross member → threshold value slightly violated
- bending longitudinal member → threshold value complied

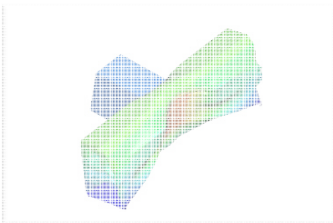
- Topometry optimization with ESL for the design of the supporting structure of an engine hood has been performed
- The result is a preliminary CAD design of the supporting structure
- In a next step nonlinear parameter optimization with LS-OPT will be performed on the basis of the preliminary CAD design to refine functional requirements
- Parameters for the optimization with LS-OPT might be gauge thickness, properties of glue lines, geometric shapes based on morphing, etc.

Agenda



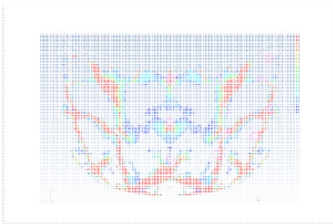
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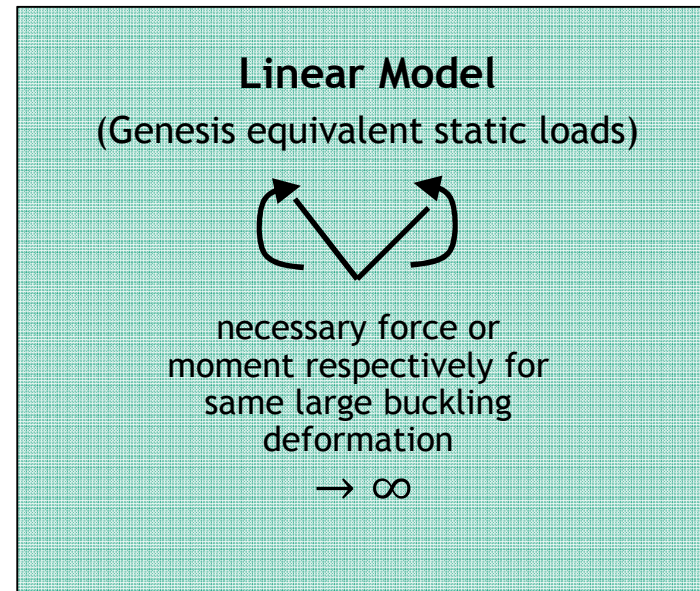
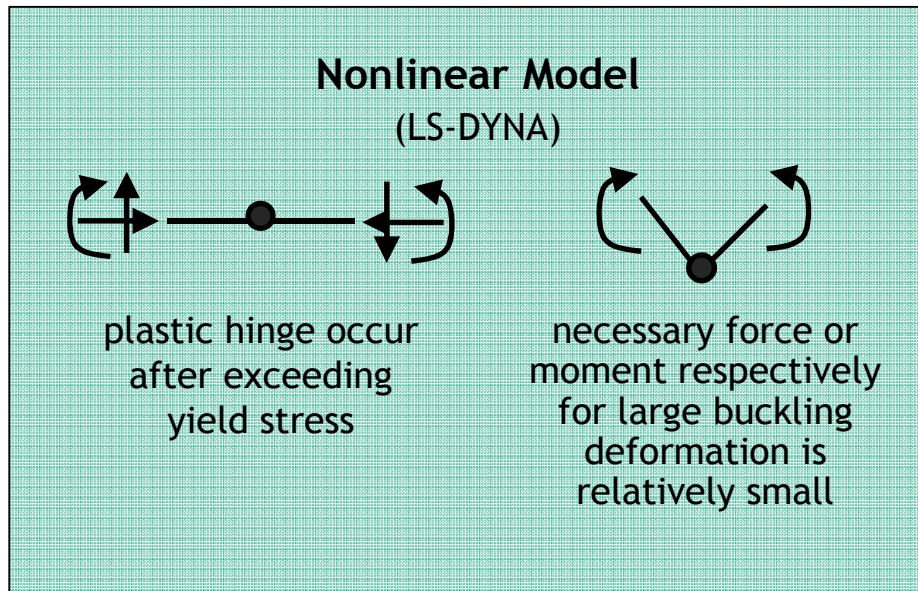
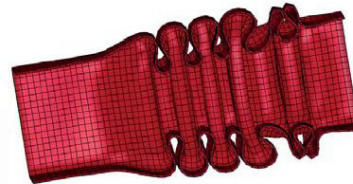
Summary

Conclusions, Lessons Learned

Conclusions

■ Limit of the ESL-Methodologie

- Local buckling/folding where plastic hinges occur leads to out of scale equivalent static loads



Conclusions

■ Formulation of Objectives

- Objectives are defined for linear optimization. This means, consideration of nonlinear responses are not directly possible
- Examples: Minimization of HIC value for head impact is not possible as an objective
- Alternative criteria have to be established

■ Formulation of Constraints

- Constraints are defined for linear optimization as well. Consideration of constraints based on nonlinear responses is not possible
- Constraints are satisfied for the linear replacement problem. They might be violated for the real nonlinear problem

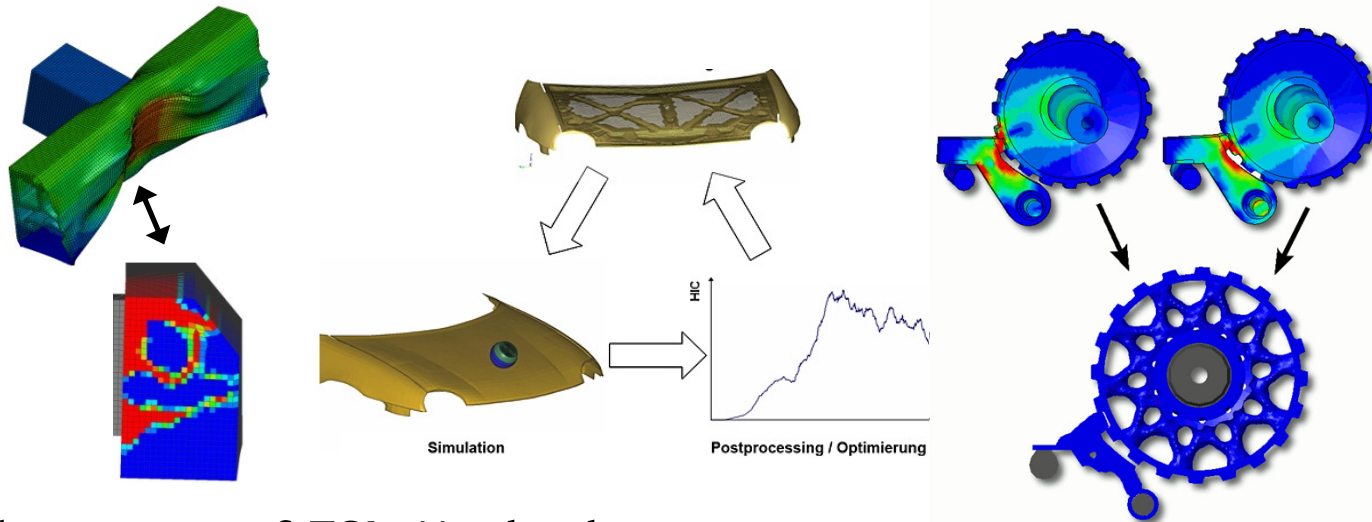
■ Automated Model Transition

- The nonlinear LS-DYNA model has to be translated to a linear Genesis model. Automation of this process is a challenging task. Many Keywords and modelling features of LS-DYNA are supported, but not 100% yet.

Conclusions

■ ESL-Method is promising

- for nonlinear applications with rather moderate deformations or with more spreaded deformations, for any contact problems, etc.
- Examples: Roof crash test, pedestrian safety load cases, pendulum impact, drop tests, gear wheels ...



■ Advantages of ESL-Method

- Enables Topology/Topometry optimization for nonlinear problems
- Size/Shape (parametric) optimization with fewer nonlinear solver calls

Thanks for your attention!

